Structural Testing of the Telling Industries, LLC
True-Bridge Clip

Report submitted to:
Telling Industries, LLC
4420 Sherwin Rd.
Willoughby, OH 44094

Report authorized by:
Rahim A. Zadeh, P.E.
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1 Introduction
Telling Industries produces a line of cold-formed steel framing members and related components including the True-Bridge Clips. These clips are used as connect lateral bridging to studs. The connections are made with self-drilling screws through the pre-drilled holes in the clip. The photograph in Figure 1-1 shows the True-Bridge Terminating and Joining Clips.

![Figure 1-1: Photograph of the True-Bridge Clips](image)

2 Objective
The objective of the work described in this report was to test combinations of the True-Bridge clips attached to different sizes of steel studs. The clips were subjected to lateral and rotational loading. These test results can be used to determine allowable loads for these connectors to be used in an engineered design.

3 Scope
A test matrix was determined based on providing a representative number of tests covering the range of products offered. Listed in Table 3-1 is the test matrix.

<table>
<thead>
<tr>
<th>Clip Type</th>
<th>Stud Size</th>
<th>Stud Thickness (mils)</th>
</tr>
</thead>
<tbody>
<tr>
<td>True-Bridge 18 ga.</td>
<td>362S162</td>
<td>68</td>
</tr>
<tr>
<td></td>
<td>600S162</td>
<td>68</td>
</tr>
<tr>
<td></td>
<td></td>
<td>97</td>
</tr>
</tbody>
</table>
4 Test Set-Up and Procedures

4.1 Test Standard
The test procedure used was developed by Telling based on industry practice for similar types of connectors.

4.2 Test Set-up
The photograph in Figure 4-1 shows the lateral loading set-up. The bridging channel was connected to a 4 ft. length of stud through the punch-out using the True-Bridge clip. The lateral load was applied with an actuator and measured with a load cell position between the actuator and the channel. The lateral deflection of the bridging channel relative to the stud was measured periodically using a digital caliper.

![Figure 4-1: Photograph Lateral Loading Test Set-Up](image)

The photograph in Figure 4-2 shows the rotational loading set-up. The bridging channel was connected to a 4 ft. length of stud through the punch-out using the True-Bridge clip. The rotational load was applied with an actuator pushing on both ends of the channel. The load was measured with a load cell positioned between each actuator and the channel. The deflection of the channel relative to the stud was measured using a displacement transducer attached to each end of the channel. The loads were applied to the channel 8 in. away from the stud. The deflections were measured at the point of load application by displacement transducers.
5 Test Results and Analysis

5.1 Test Results
The plots of the rotational load tests are given in Figures 5-1 and 5-2 for the 362S162 and 600S162 stud sizes respectively. The plots of the lateral load tests are given in Figures 5-3 and 5-4 for the 362S162 and 600S162 stud sizes respectively.
Figure 5-1: Rotational Loading Plots for 362S162 Studs

Figure 5-2: Rotational Loading Plots for 600S162 Studs
Figure 5-3: Lateral Loading Plots for 362S162 Studs

Figure 5-4: Lateral Loading Plots for 600S162 Studs
5.2 Calculation of the Safety Factor

The tested strengths are required to be reduced by a safety factor, \( \Omega \), determined in accordance with the provisions of AISI S100 using the statistical parameters based on “Other Connections and Fasteners”. The first step is to determine the resistance factor using Eq. 5-1 reproduced from S100.

\[
\phi = C_\phi \left( M_m F_m P_m \right) e^{-\beta_0 \sqrt{V_M^2 + V_F^2 + C_P V_P^2 + V_Q^2}}
\]

Eq. 5-1

where,
- \( C_\phi = 1.52 \)
- \( M_m = 1.0 \)
- \( F_m = 1.0 \)
- \( P_m = 1.0 \)
- \( \beta_0 = 2.5 \)
- \( V_M = 0.10 \)
- \( V_F = 0.05 \)
- \( C_P = (1 + 1/n)m/(m-2) \) for \( n \geq 4 \)
- \( n = \) number of tests
- \( m = \) degrees of freedom = \( n-1 \)
- \( V_P = \) COV of test results \( \geq 0.065 \)
- \( V_Q = 0.21 \)

Once the resistance factor is determined using Eq. 5-1, the corresponding safety factor is calculated as follows:

\[
\Omega = 1.6/\phi
\]

Eq. 5-2

6 Allowable Loads

6.1 Allowable Loads and Stiffness for Rotational Loading

The allowable rotational loads for the 18-gauge True-Bridge clip connecting a 16-gauge bridging channel to the various stud sizes are given in Table 6-1. The rotational stiffnesses for these same connections are given in Table 6-2. The stiffness is calculated based on the average of deflection divided by the load for all data points shown in Figures 5-1 and 5-2.

<table>
<thead>
<tr>
<th>CFS Member</th>
<th>Ultimate Moment (in-lbs)</th>
<th>COV</th>
<th>( \Omega )</th>
<th>Allowable (in-lbs)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Test #1</td>
<td>Test #2</td>
<td>Test #3</td>
<td>Average</td>
<td></td>
</tr>
<tr>
<td>362S162-68</td>
<td>1197</td>
<td>1146</td>
<td>1162</td>
<td>1168</td>
</tr>
<tr>
<td>362S162-97</td>
<td>1668</td>
<td>1656</td>
<td>1620</td>
<td>1648</td>
</tr>
<tr>
<td>600S162-68</td>
<td>1193</td>
<td>1314</td>
<td>1277</td>
<td>1261</td>
</tr>
<tr>
<td>600S162-97</td>
<td>2086</td>
<td>1936</td>
<td>2013</td>
<td>2011</td>
</tr>
</tbody>
</table>
### Table 6-2: Rotational Stiffness

<table>
<thead>
<tr>
<th>CFS Member</th>
<th>Stiffness (in-lbs/radian)</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Test #1</td>
<td>Test #2</td>
</tr>
<tr>
<td>362S162-68</td>
<td>5112</td>
<td>4642</td>
</tr>
<tr>
<td>362S162-97</td>
<td>6990</td>
<td>6697</td>
</tr>
<tr>
<td>600S162-68</td>
<td>4029</td>
<td>4019</td>
</tr>
<tr>
<td>600S162-97</td>
<td>7327</td>
<td>7065</td>
</tr>
</tbody>
</table>

### 6.2 Allowable Loads and Stiffness for Lateral Loading

The allowable lateral loads for the 18-gauge True-Bridge clip connecting a 16-gauge bridging channel to the various stud sizes are given in Table 6-3. The lateral stiffnesses for these same connections are given in Table 6-4. The stiffness is calculated based on the deflection divided by the load at approximately 50% of the ultimate load.

#### Table 6-3: Allowable Lateral Loads

<table>
<thead>
<tr>
<th>CFS Member</th>
<th>Ultimate Load (lbs)</th>
<th>COV</th>
<th>Ω</th>
<th>Allowable (lbs)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Test #1</td>
<td>Test #2</td>
<td>Test #3</td>
<td>Average</td>
</tr>
<tr>
<td>362S162-68</td>
<td>1224</td>
<td>1270</td>
<td>1309</td>
<td>1268</td>
</tr>
<tr>
<td>362S162-7</td>
<td>1562</td>
<td>1516</td>
<td>1527</td>
<td>1535</td>
</tr>
<tr>
<td>600S162-68</td>
<td>1311</td>
<td>1252</td>
<td>1372</td>
<td>1312</td>
</tr>
<tr>
<td>600S162-7</td>
<td>2233</td>
<td>2298</td>
<td>2367</td>
<td>2299</td>
</tr>
</tbody>
</table>

#### Table 6-4: Lateral Stiffness

<table>
<thead>
<tr>
<th>CFS Member</th>
<th>Stiffness (lbs/in) at 0.5 P&lt;sub&gt;ult&lt;/sub&gt;</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Test #1</td>
<td>Test #2</td>
</tr>
<tr>
<td>362S162-68</td>
<td>1474</td>
<td>1058</td>
</tr>
<tr>
<td>362S162-7</td>
<td>2348</td>
<td>1824</td>
</tr>
<tr>
<td>600S162-68</td>
<td>1275</td>
<td>1505</td>
</tr>
<tr>
<td>600S162-7</td>
<td>1915&lt;sup&gt;1&lt;/sup&gt;</td>
<td>4962</td>
</tr>
</tbody>
</table>

<sup>1</sup> These values were considered outliers and not included in the average.